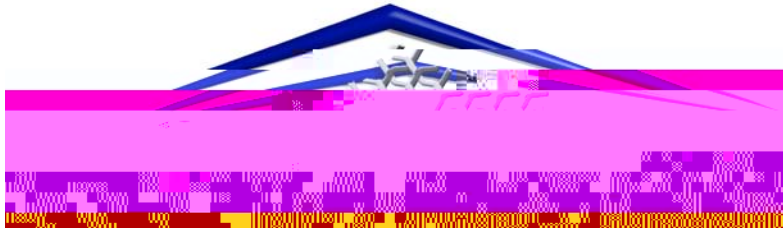


FYdcfh'Bc.'75A!FD!&\$%-!\$( )'FYj'B#7''  
FYdcfh'8UhY.'8YWY a VYf' %-ž&\$%-

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- 



Gc`jUm'fl : cf a Yf`m'7mhYWL`)'&\$!%'H\* )\$' '\_!DK`  
ZUVf]W'k]h\`' \* i`F7`  
9e i]jU`YbWm`AUhYf]U`DfcdYfhm'8UhU'FYdcfh`  
Zcf`@U a ]bUhY'FYdU]f'DfYdfY[ `6UhW\`

B75AD'Dfc^YWh`Bi a VYf.'BDB`\$'%, \$%'

B75AD'HYgh'FYdcfh`Bi a VYf.'75A!FD!&\$%-!\$( )'FYj'B#7

FYdcfh'8UhY.'8YWY a VYf' %-ž&\$%-`

HYgh]b[ ` : UW]`]hm.`

National Institute for Aviation Research  
Wichita State University  
1845 N. Fairmount  
Wichita, KS 67260-0093

HYgh'DUbY` : UVf]WUh]cb` : UW]`]hm.`

National Institute for Aviation Research - NCAT  
Wichita State University  
4004 North Webb Road  
Wichita, KS 67226

8]ghf]V i h]cb`GhUhY a Ybh`5" Approved for public release; distribution is unlimited.

5HSRUW 1R &\$0 53  
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5HY 1

3UHSDUHG E\

(YHO\Q /LDQ

5HYLHZHG E\

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%"% GWcdY`

The test methods and results described in this document are intended to provide basic composite properties essential to most methods of analysis and are consistent with CMH-17-1G—Composite Materials Handbook for Polymer Matrix Composites. This report contains material property data of common usefulness to wide range of projects. The lamina and laminate material property data have been generated with NCAMP oversight in accordance with NSP 100 NCAMP Standard Operating Procedures; the test panels and test specimens have been inspected by NCAMP Authorized Inspection Representatives (AIR) and the testing has been witnessed by NCAMP Authorized Engineering Representatives (AER). However, the data may not fulfill all the needs of any specific company's program; specific properties, environments, laminate architecture, and loading situations may require additional testing.

The use of NCAMP material and process specifications does not guarantee material or structural performance. Material users should be actively involved in evaluating material performance and quality including, but not limited to, performing regular purchaser quality control tests, performing periodic equivalency/additional testing, participating in material change management activities, conducting statistical process control, and conducting regular supplier audits.

The applicability of NCAMP material property data, material allowables, and specifications must be evaluated on a case-by-case basis by aircraft companies and certifying agencies. NCAMP assumes no liability whatsoever, expressed or implied, related to the use of the material property data, material allowables and specifications.

This report contains material property data only. Equivalency statistical analysis data is given in NCP-RP-2018-017 Rev N/C and engineering basis values generated from material qualification testing can be obtained from NCP-RP-2012-023 Rev N/C or later revisions. The equivalency material was procured to NCAMP Material Specification NMS 532/6 Rev A Release dated September 19, 2016. The equivalency test panels were cured in accordance with NCAMP Process Specification NPS 85321 Revision C dated May 31, 2018 Baseline "C" Cure Cycle. The NCAMP Test Plan NTP 5325QR1 was used for this equivalency program.

Part fabricators that wish to utilize the material property data, allowables and specifications may be able to do so by demonstrating the capability to reproduce the original material properties; a process known as equivalency. More information about this equivalency process including the test statistics and its limitations can be found in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G. The applicability of equivalency process must be evaluated on program-by-program basis by the applicant and certifying agency. The applicant and certifying agency must agree that the equivalency test plan, along with the equivalency process described in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G, are adequate for the given program.

Aircraft companies should not use the data published in this report without specifying NCAMP Material Specification NMS 532/6. NMS 532/6 have additional requirements that are listed in its prepreg process control document (PCD), fiber specification, fiber PCD and other raw material specifications and PCDs which impose essential quality controls on the raw materials and raw material manufacturing equipment and processes. Aircraft companies and certifying agencies should assume that the material property data published in this report is not applicable when the material is not procured to NMS 532/6. NMS 532/6 is a free, publicly available, non-proprietary aerospace industry material specification.

The data in this report is intended for general distribution to the public, either freely or at a price that does not exceed the cost of reproduction (e.g. printing) and distribution (e.g. postage).

**%"&` Gma Vc`g`**

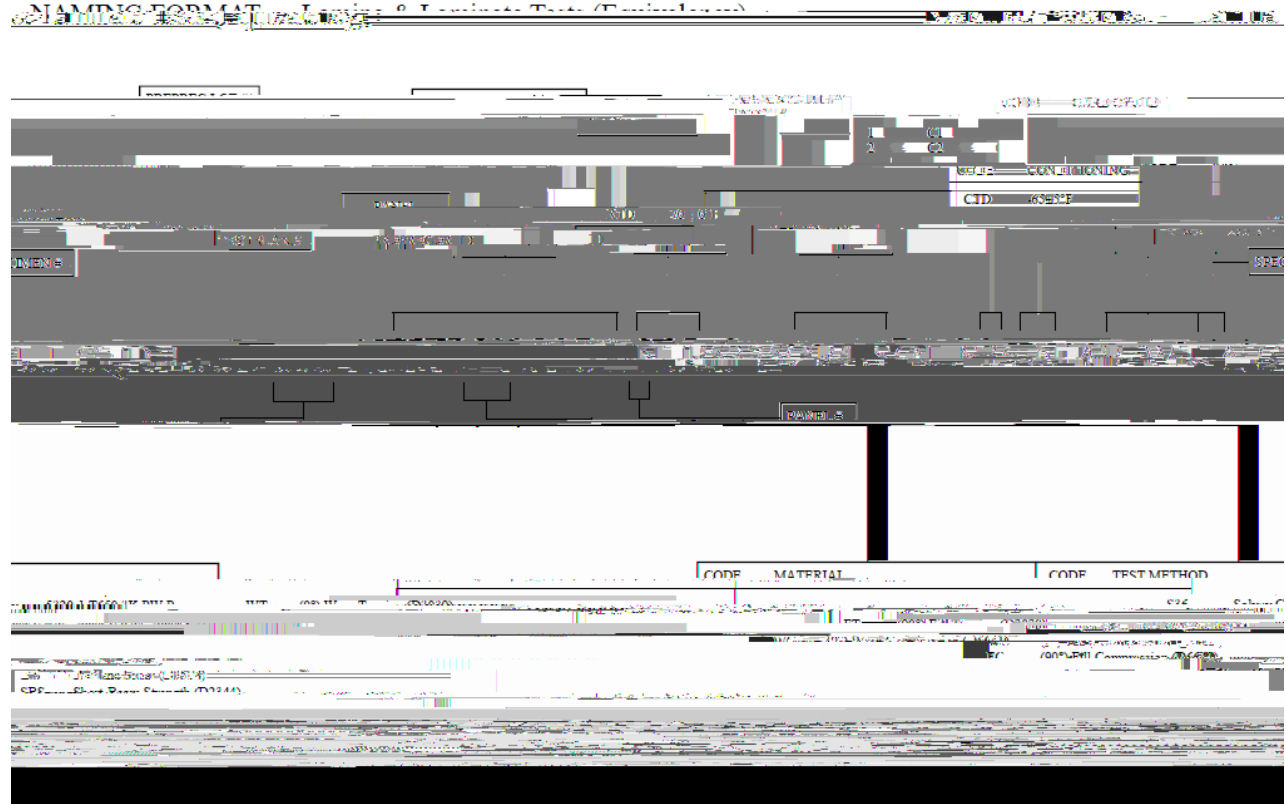
$\nu^t$	major Poisson's ratio, tension
P H	micro-strain
$E_1^c$	compressive modulus, longitu



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%"'' B=5 FEGdYW]a Yb'BU a]b[': cf a Uh'



:][ i fY'%!%. 'AUhYf]U'BU a]b[': cf a Uh'



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%"(' FYZYfYbWYg'

5GHA'GhUbXUfXg'

All testing was in accordance

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%" )' AYh\cXc`c [m`

%" )"%' DfcWYgg`8YZ]b]h]cb`

A single batch of prepreg was used to demonstrate equivalency. These single batch tests are designed to demonstrate equivalency with the original three batches qualification data for purposes described in CMH-17-1G Section 8.4.1 and DOT/FAA/AR-03/19 Section 6.

For each combination of test, batch and condition, the specimens were selected from a minimum of two separate panels cured separately as shown in Figure 1-2 unless



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%)"&`GdYW] a Yb` /`HYgh]b [ `8YhU]`g`

%)"&%"`HUVV]b [ `

Tabs were not used for this program.

%)"&`&`

%" )"'HYgh' AUhf]I'

The table below shows lay-ups and test matrices used for lamina and laminate level testing on the single batch equivalency of the Solvay 5320-1 T650 3k PW prepreg material.

Layup	Test Type and Direction	Property	Number of Batches x Number of Panels x Number of Specimens		
			Test Temperature/ Moisture Condition		
			CTD	RTD	ETW2
[0] <sub>15</sub>	ASTM D3039 Warp Tension	Strength, Modulus and Poisson's Ratio	1x2x4	1x2x4 (4)	1x2x4
[0] <sub>15</sub>	ASTM D6641 Warp Compression	Strength, Modulus and Poisson's Ratio	1x2x4	1x2x4 (1)(4)	1x2x4 (3)
[90] <sub>15</sub>	ASTM D3039 Fill Tension	Strength and Modulus	1x2x4	1x2x4 (4)	1x2x4
[90] <sub>15</sub>	ASTM D6641 Fill Compression	Strength and Modulus	1x2x4	1x2x4 (1)(4)	1x2x4 (3)
[45/-45] <sub>3S</sub>	ASTM D3518 In-Plane Shear (2)	Strength and Modulus	1x2x4	1x2x4 (4)	1x2x4
[0] <sub>32</sub>	ASTM D2344 Short Beam	Strength	1x2x4	1x2x4	1x2x4
(25/50/25 - QI) [45/0/-45/90]2S	ASTM D5766 Open-Hole Tension	Strength		1x2x4	1x2x4
(25/50/25 - QI) [45/0/-45/90/45/0/- 45/90/-45/90]S	ASTM D6484 Open-Hole Compression (5)	Strength		1x2x4 (1)	1x2x4
(25/50/25 - QI) [45/0/-45/90]3S	ASTM D7136 & D7137 Compression After Impact (1500 in/lb/in)	Strength		1x2x4	

HUV'Y'!%. '9e i]jU'YbWm'HYgh' AUhf]I'

**BchY'.** Back-to-back strain gages are needed on the first two specimens. If no buckling is observed, the remaining modulus specimens will require a strain gage on one side of the specimens only. An appropriate extensometer may be used in place of the strain gage.

**BchY'&.** Gripped (tab) length is 1.5±0.5" on each end of the 10" long specimen. Once the samples have reached the 5% strain level, the actuator/crosshead displacement rate can be increased by four times the initial rate. Continue testing at the higher strain rate until ultimate failure is observed.

**BchY'.** If strain gage is used for modulus measurement, a separate un-gaged specimen must be used for strength measurement; because the strain gage and its protective coating may prevent moisture absorption in the gage area.

**BchY' (.** At least two specimens must be gaged to obtain full stress-strain curve to failure. An appropriate extensometer may be used in place of the strain gage for the remaining specimens.

**BchY' ).** Open-hole configuration: 0.25" hole diameter, 1.5" width.

**8YWy a VYf %-ž&\$%-' . . . . . '75 A!FD!&\$%-!\$( )'FYj'B#7**

Table 1-1 shows the single batch of the Solvay 5320-1 T650 3k PW prepreg test matrix. The layup angles 0°, 45°, -45° and 90° refer to the orientation of the warp direction. The laminate stacking sequences in this program are not specific to any design. Therefore, careful consideration should be given to the validity of properties derived from this program based on the design specific laminates in a structure to be certified.

**%)" ('7 i fYX'@U a ]bUhY'D \mg]WU'`HYgh]b [ '**

The properties in Table 1-2 were determined for each panel used for test coupons with the exception of Tg by DMA which were conducted on one laminate per batch from each oven cure conducted where that batch is present. The tests were performed by the National Institute for Aviation Research (NIAR) Composites Laboratory under the supervision of NCAMP.

**DfcdYfhm'**

**7cbX]h]cb#AYh \cX'**

8YWY a VYf %-ž&\$%- . . . . . \*\*\*\*\*75 A!FD!&\$%-!\$( )`FYj`B#7

%")")`9bj]fcb a YbhU`7cbX]h]cb]b[`

The following tests were performed by the NIAR Composites Laboratory under the supervision of NCAMP.

Test environments are defined as:

- CTD = -65±5°F, dry
- RTD = 70±10°F, dry
- ETW2 = 250±5°F, wet

Within each test method and test environment, the failure mode was evaluated immediately after each test by an NCAMP staff engineer or NCAMP AER. All tested

%" )"\*' Bcb!U a V]Ybh'HYgh]b [ '

The chamber was of adequate size so that all test fixtures and load frame grips were contained within the chamber.

For elevated temperature testing, the temperature chamber, test fixture, and grips were preheated to the specified temperature. Each specimen was heated to the required test temperature as verified by a thermocouple in direct contact with and taped to the specimen gage section. The heat-up time of the specimen did not exceed 5 minutes, unless otherwise specified in individual test summary sheets. The test was started 5 <sup>1</sup>/<sub>0</sub> minutes after the specimen reached the test temperature. During the test, the temperature, as measured on the specimen, was within 5°F of the required test temperature.

For subzero temperature testing, each specimen was cooled to the required test temperature as verified by a thermocouple in direct contact with and taped to the specimen gage section. The test started 5 <sup>1</sup>/<sub>0</sub> minutes after the specimen reached the test temperature. During the test, the temperature, as measured on the specimen, was within 5°F of the required test temperature.

For wet specimens, the moisture loss was determined by subjecting representative specimens to the same amount of time required to heat-up and fail the specimens. For filled-hole or bearing specimens, fasteners were removed prior



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%)"+'Bcf a U`nUh]cb'DfcWYX i fYg'

Most lamina level tension and compression strength and modulus properties, and all laminate level properties were normalized according to nominal cured ply thickness. Lamina level properties that were not normalized include 90° tensile strength and modulus (unidirectional only), 90° compressive strength and modulus (unidirectional only), in-plane shear strength and modulus, Poisson's ratio, SBS, and ILT. After normalizing, data scatter reduced or remained the same. If data scatter increased significantly after normalizing, the reason was investigated. Wherever properties are normalized, both measured and normalized data were reported.

The average cured ply thickness of 0.0077 inches has been used as the nominal cured ply thickness (CPT) for normalization purpose. This value was used in the normalization of data in the qualification program. The following normalization formula was used:

Normalized Value = Measured Value x Measured CPT / Nominal CPT.

%)", '=bgdYWh]cb' JYf]Z]WUh]cb'

The 1-batch equivalency panels have been fabricated according to the requirements of the test plan and conformed by an NCAMP AIR. The test specimens and test setup have also been conformed by an NCAMP AIR.

Testing was witnessed by NCAMP. Test setup and witnessing was delegated to an NCAMP AER. Mechanical testing was carried out at the National Institute for Aviation Research, Wichita State University.

%)"- 'AUhYf]U`DYX] [fYY'=bZcf a Uh]cb'

The PMC Data Collection Template includes the material pedigree information required, such as material and batch information, as well as panel fabrication record, environmental conditioning, test equipment, and test procedures.

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&"` HYgh`FYg i`hg`

&"%` @Ua ]bU`@YjY``HYgh`G i a a Ufm`

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )`FYj`B#7

&"'' =bX]j]X i U`HYgh'G i a aUf]Yg`

&" "%' KUfd'HYbg]cb'DfcdYfh]Yg'flKHL`

AUhYf]U` Solvay 5320-1 T650 3k-PW fabric with 36% RC						<b>HYbg]cbž%!U]jg`</b> Solvay 5320-1 T650 3k-PW fabric with 36% RC [0]15	
FYg]b`Wcb]Ybh. :]VYf`jc`i aY. D`m`Wc`i bh.	37.53 %wt 54.83 %vol 15	7ca d`XYbg]hm. 1.553 g/cc					
HYgh`a Yh`cX. BcfaU]nYX`Vm.	ASTM D3039-17 0.0077 in. CPT	AcXi`ig`WU`Wi`Uh]cb. 1000-3000 microstrain					
		7H8	FH8		9HK&		
HYgh`HY a dYf]Uh`i fY`š:0 Ac]gh`i fY`7cbX]h]cb]b[ 9e`i]Vf]i a`Uh`H`F< Gc`i fWY`WcXY`dfYZ]iYX`Vm.NTP-5325QRI-SOL-S36-NIAR-		-65 Dry WT-X-CX-1-CTD-X	70 Dry WT-X-CX-1-RTD-X		250 Equilibrium 160 F,85% WT-X-CX-1-ETW2-X		
		BcfaU]nYX`	AYUg`i fYX`	BcfaU]nYX`	AYUg`i fYX`	BcfaU]nYX`	AYUg`i fYX`
AYUb A]b]a i a AU]a i a 7`J`fi l`		108.021 105.173 111.779 2.222	109.315 106.713 113.515 2.238	121.316 118.808 124.669 1.662	122.606 119.498 126.754 1.929	135.410 129.038 140.538 2.473	136.203 130.257 142.805 2.774
Bc`GdY]a Ybg Bc`DfYdfY[ `@c]g		8 1	9 1		16 1		
AYUb A]b]a i a AU]a i a 7`J`fi l`		9.806 9.728 9.908 0.637	9.923 9.838 10.062 0.717	9.755 9.663 9.902 0.688	9.858 9.775 10.068 0.948	9.751 9.487 9.971 1.483	9.809 9.456 10.140 2.253
Bc`GdY]a Ybg Bc`DfYdfY[ `@c]g		8 1	9 1		16 1		
AYUb A]b]a i a AU]a i a 7`J`fi l`		0.054 0.049 0.060 7.419	0.049 0.042 0.055 7.228		0.046 0.034 0.051 11.600		
Bc`GdY]a Ybg Bc`DfYdfY[ `@c]g		8 1	9 1		8 1		

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )`FYj`B#7

8YWy a VYf %-ž&\$%- .....75A!FD!&\$%-!\$( )'FYj'B#7

&"'''' KUfd'7c a dfYgg]cb'DfcdYfh]Yg'fl K 7Ł'

AUyYfJU'.

FYgjb'WcbhYbh. 37.60 %wt





&"")'=b!D`UbY`G\YUf`DfcdYfh]Yg`fl=DGL`

AUhYfjU`.

FYgjb`WcbhYbh. 37.09 %wt  
:jVYf`jc`i aY. 55.12 %vol  
D`m`Wc i bh. 12

7c a d`XYbg]hm. 1.551 g/cc

HYgh`a Yh\cX. ASTM D3518-18

AcXi`i`g`WU`Wi`U]jcb.` 2000-6000 microstrain

BcfaU`]nYX`Vm. NA

	BcfaU`]nYX	AYUg ifYX	BcfaU`]nYX	AYUg ifYX	BcfaU`]nYX	AYUg ifYX
AYUb		11.536		8.322		3.523
A]b]a i a		11.169		8.230		3.434
AU]a i a		11.788		8.415		3.633
7`J`fi i Ł		1.703		0.630		1.870
<b>Bc`GdY]a Ybg</b>						
<b>Bc`DfYdfY[`@chg</b>						
AYUb		18.308		14.455		6.712
A]b]a i a		17.843		14.289		6.549
AU]a i a		18.761		14.700		6.968
7`J`fi i Ł		2.137		0.835		2.182
<b>Bc`GdY]a Ybg</b>						
<b>Bc`DfYdfY[`@chg</b>						
AYUb		0.847		0.726		0.365
A]b]a i a						





8YWy a VYf %-ž&\$%-`

8YWy a VYf %-ž'&\$%-

.....75 A!FD!&\$%-!\$( )'FYj'B#7

&"'+ Í&)#)\$&) Î`CdYb!<c`Y`HYbg]cb`%`DfcdYfh]Yg`flC<H%L`

AUhYfjU` Solvay 5320-1 T650 3k-PW fabric with 36% RC				<b>CdYb!&lt;c`Y`HYbg]cb`%</b> Solvay 5320-1 T650 3k-PW fabric with 36% RC [45/0-/45/90]2S	
FYgjb`WcbhYbh. 37.65 % wt :jVYf`jc`i aY. 54.40 % vol D`m`Wc i bh. 16	7ca d`XYbg]hm. 1.544 g/cc				
HYgh`a Yh\cX. ASTM D5766-11					
BcfaU`nYX`Vm. 0.0077 in. CPT					
	<b>FH8</b>		<b>9HK&amp;</b>		
HYgh`HY a dYfUhi fY`0s :0 AcjghifY`7cbX]cb]b[ 9ei`]Vf]i a`Uh`H`F< Gc ifWY`WcXY`dfYz]lYX`Vm. NTP-5325QRI-SOL-S36-NIAR-	70 Dry		250 Equilibrium 160 F,85%		
	OHT1-X-CX-1-RTD-X		OHT1-X-CX-1-ETW2-X		
	<b>BcfaU`nYX</b>	<b>AYUg ifYX</b>	<b>BcfaU`nYX</b>	<b>AYUg ifYX</b>	
AYUb A]b]a i a AU]a i a C<H%`GhfYb [h\`0_g] 7`J`i i L	43.951	43.910	48.089	48.046	
	40.550	40.534	46.157	46.151	
	46.590	46.634	49.744	49.663	
	4.420	4.457	2.929	2.874	
Bc`GdY]a Ybg Bc`DfYdfY[`@chg	8 1		8 1		

&"", 'Í&)#)\$&)Î`CdYb!<c`Y`7c a dfYgg]cb`%`DfcdYfh]Yg`flC<7%L`

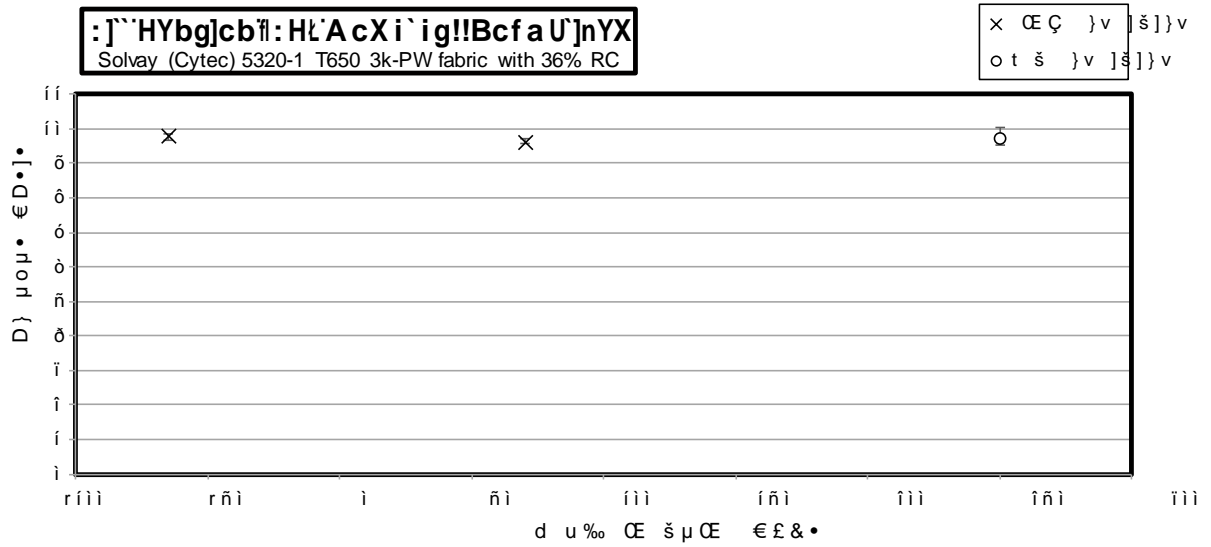
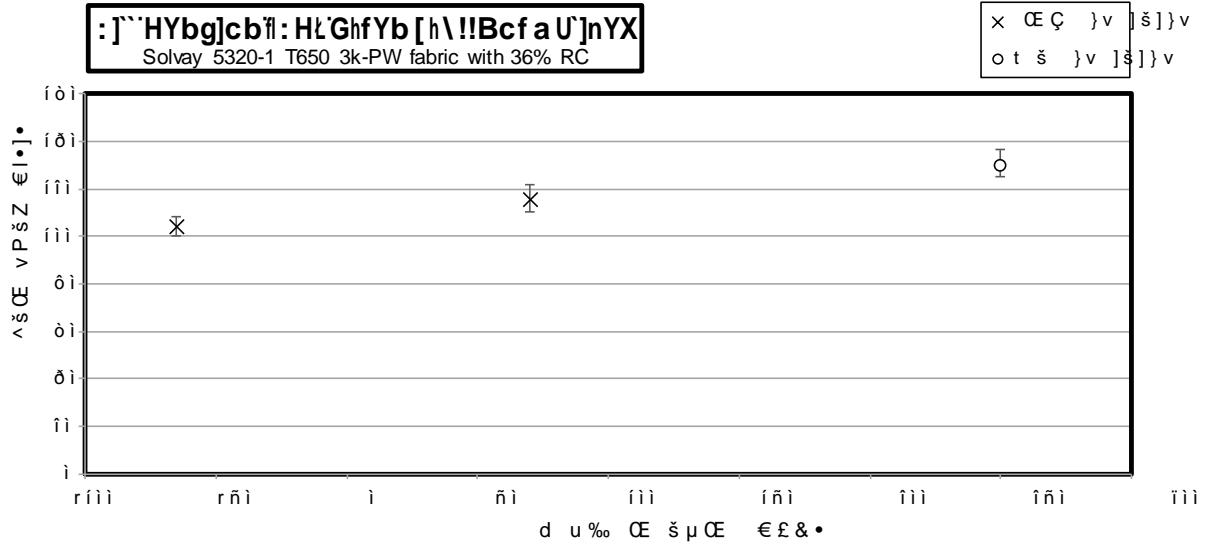
AUhYfJU` Solvay 5320-1 T650 3k-PW fabric with 36% RC				<b>CdYb!&lt;c`Y`7c a dfYgg]cb`%</b> Solvay 5320-1 T650 3k-PW fabric with 36% RC [45/0/-45/90/45/0/-45/90/-45/90]S	
FYgjb`WcbhYbh. 37.47 %wt :jVYf`jc`i aY. 54.59 %vol D`m`Wc i bh. 20	7c a d`XYbg]hm. 1.545 g/cc				
HYgh`a Yh\cX. ASTM D6484-14					
BcfaU`nYX`Vm. 0.0077 in. CPT					
	<b>FH8</b>		<b>9HK&amp;</b>		
HYgh`HY a dYfUhi fY`S:Q AcjghifY`7cbX]cb]b[ 9ei`]Vf]i a`Uh`H`F< Gc i fWY`WcXY`dfYz]iYX`Vm. NTP-5325QRI-SOL-S36-NIAR-	70 Dry		250 Equilibrium 160 F,85%		
	OHC1-X-CX-1-RTD-X		OHC1-X-CX-1-ETW2-X		
	<b>BcfaU`nYX`</b>	<b>AYUg ifYX`</b>	<b>BcfaU`nYX`</b>	<b>AYUg ifYX`</b>	
AYUb A]b]a i a AU]a i a C<7%GhYb[h\`0_g] 7`J`i L	48.841	48.733	34.424	34.331	
	47.549	47.462	32.504	32.316	
	50.365	50.099	36.655	36.568	
	1.718	1.623	3.808	3.830	
Bc`GdY]a Ybg Bc`DfYdfY[`@chg	8 1		8 1		

8YWy a VYf %-ž&\$%-`

8YWy a VYf %-ž&\$%-

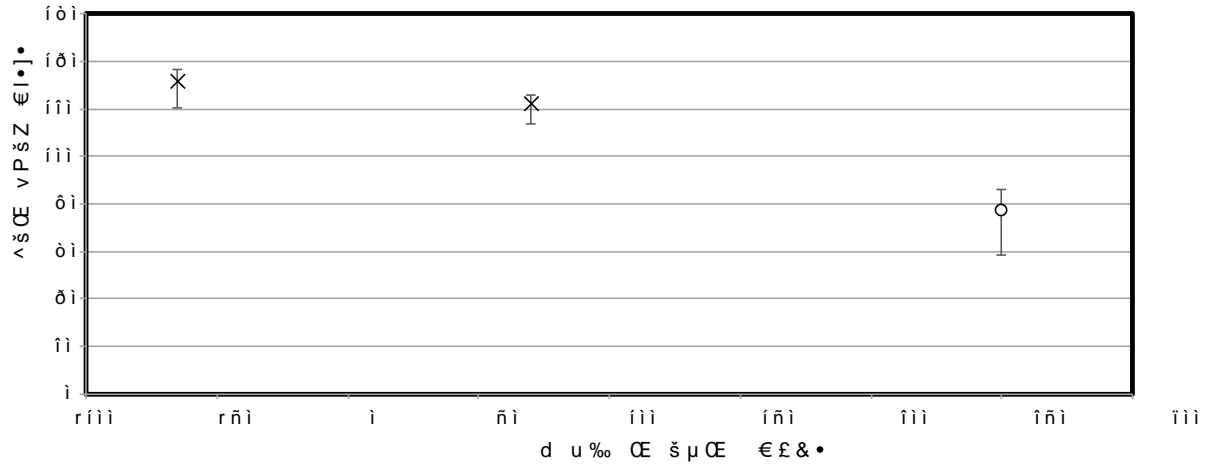
.....75A!FD!&\$%-!\$( )`FYj`B#7

'"&' :j''HYbg]cb'DfcdYfh]Yg'fl:Hk'



'"' K Ufd'7c a dfYgg]cb'DfcdYfh]Yg'flK 7Ł'

**KUfd'7c a dfYgg]cb'flK 7Ł'GhfYb [h\!!Bcf aU`nYX**  
Solvay 5320-1 T650 3k-PW fabric with 36% RC



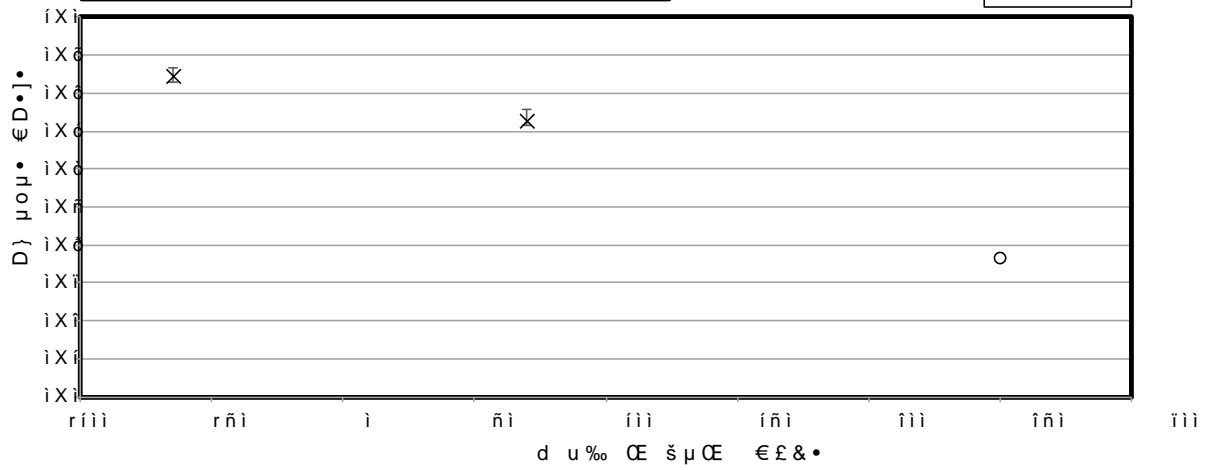




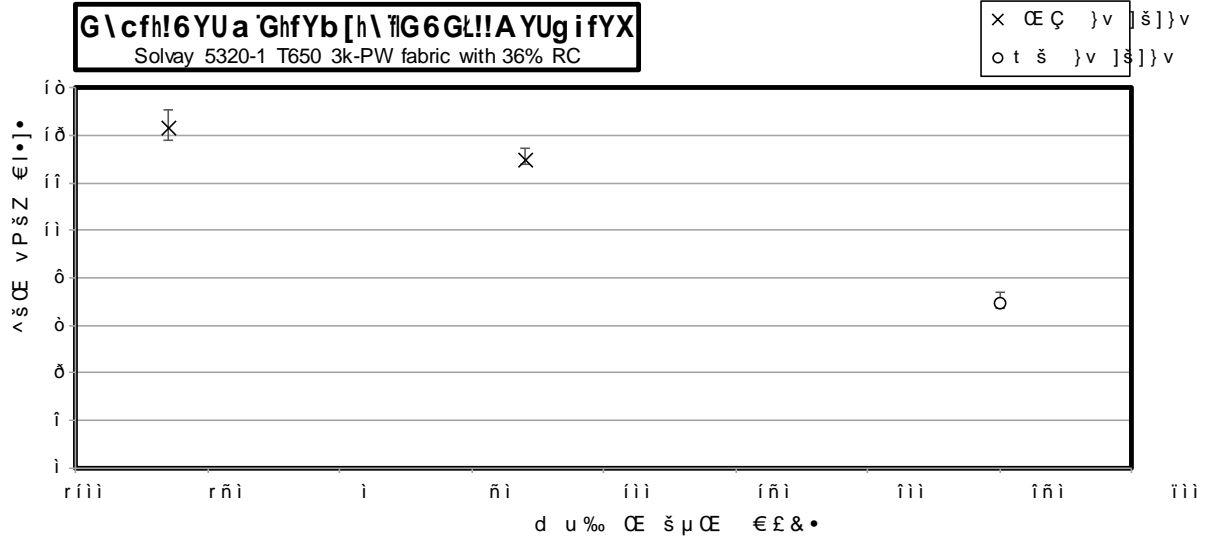


**=b!D`UbY`G\YUfñ=DGL`AcXi`ig!!AYUgi fYX**  
Solvay 5320-1 T650 3k-PW fabric with 36% RC

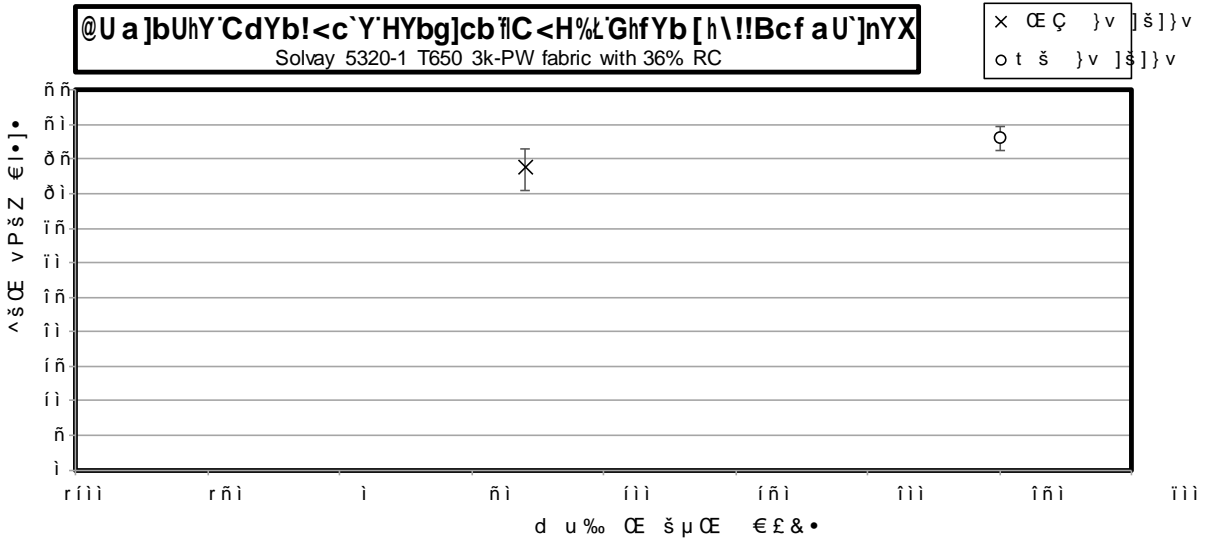
x œ ç }v ]š}}v  
o t š }v ]š}}v



'\*\*' @U a ]bU'G\cfh!6YU a 'GhfYb [h\ 'DfcdYfh]Yg'flG6GŁ'



'"+' Í&#)\$#&)Î'CdYb!<c`Y'HYbg]cb`%'DfcdYfh]Yg'flC<H%Ł'





8YWy a VYf %-ž&\$%- .....75A!FD!&\$%-!\$( )'FYj'B#7

(" FUK'8UhU'

("% K Ufd'HYbg]cb'DfcdYfh]Yg'fl KHL'

b c f a U ] n ] b [ '  
h d e



8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )'FYj`B#7

bcf a U'n]b [  
h<sub>d</sub>m '0]b0  
0.0077

GdYw]a Yb`B i a VYf

B-5F`  
6UwV\`

B-5F`





8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )'FYj'B#7

bcaU'n]b[  
h<sub>ca</sub>'0]b0  
0.0077

GdYw]a Yb'Bi a VYf	B-5F' 6UhW\`	B-5F' 7 ifY'7mWY	DfydfY['@ch'	7 ifY'7mWY'	GfYb[h\ 0_g]0	AcX1' ig' 0Ag]0	Dc]ggcblg' FUh]c	5 j[' GdYw]a Yb' H\]W_bYgg' 0]b0	'D]Yg]b' @Ua]bUhY	:U] ifY' AcXY	5 j['h <sub>ca</sub> '0]b0	GfYb[h\ 0_g]0	AcX1' ig' 0Ag]0
NTP-5325QRI-SOL-S36-NIAR-WT-A-C1-1-ETW2-1*	A	C1	1	1	130.488	10.083		0.114	15	LGB	0.0076	129.038	9.971
NTP-5325QRI-SOL-S36-NIAR-WT-A-C1-1-ETW2-2*	A	C1	1	1	142.794	9.946		0.114	15	LGB	0.0076	140.404	9.780



("&' :]'`HYbg]cb'DfcdYfh]Yg'fl : HŁ'

:]'`HYbg]cb'DfcdYfh]Yg'fl : HŁ!!7H8  
 GhfYb[h\`/'AcXi`ig  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

bcf a U'n]b[  
 hcfm'0]b0  
 0.0077

GdYW]aYb Bi a VYf	B:5F' 6UHw\`	B:5F' 7iFY'7mWY	DfYdfY['@ch`	7iFY'7mWY	GhfYb[h\ 0_g]0	AcXi`ig' 0Ag]0	5j['` GdYW]aYb' H\]W_bYgg' 0]b0	'D]Yg]b' @Ua]bUhY	:U] ifY'AcXY	5j['`hcfm'0]b0	GhfYb[h\bcfa' 0_g]0	AcXi`igbcfa' 0Ag]0
NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-1	A	C1	1	1	103.236	9.953	0.114	15	LGT	0.0076	102.089	9.842
NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-2	A	C1	1	1	105.968	9.986	0.114	15	LGM	0.0076	104.790	9.875
NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-3	A	C1	1	1	106.253	9.974	0.114	15	LGB	0.0076	104.827	9.840
NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-4	A	C1	1	1	106.223	9.938	0.114	15	LGM	0.0076	104.721	9.797
NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-1	A	C2	1	2	101.153	9.780	0.116	15	LAB	0.0077	101.474	9.811
NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-2	A	C2	1	2	107.948	9.816	0.116	15	LGM	0.0077	108.229	9.842
NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-3	A	C2	1	2	107.751	9.671	0.115	15	LGB	0.0077	107.580	9.656
NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-4	A	C2	1	2	99.708	9.738	0.116	15	LGB	0.0077	100.111	9.778

5jYfU[Y	%'(+,\$	-',)+	5jYfU[Ybcfa	\$\$S++	%'&& ,	-',)\$
GhUbXUfX'8Yj'	''\$**	%'&&	GhUbXUfX'8Yj'bcfa		&'*\$	\$\$\$,
7cYZZ'cZ'JUf'0 i 0	&'&*	%'&&+	7cYZZ'cZ'JUf'0 i 0bcfa		&'+(	\$\$-\$
A]b'	--+\$,	--+*	A]b'	\$\$\$+*	\$\$\$%%	-')*
AUI'	%'+'-(,	-',)*	AUI'	\$\$\$++	%'&&-	-',)+
Bi a VYf cZ'GdYW'	,	,	Bi a VYf cZ'GdYW'	,	,	,



8YWy aVYf %-z`&\$%- ' . . . . . \*75A!FD!

:]``HYbg]cb'DfcdYfh]Ygřl: Hł!!FH 8  
Bcf a U`]nYX'GhfYb [h\



8YWy a VYf %-ž'&\$%-'





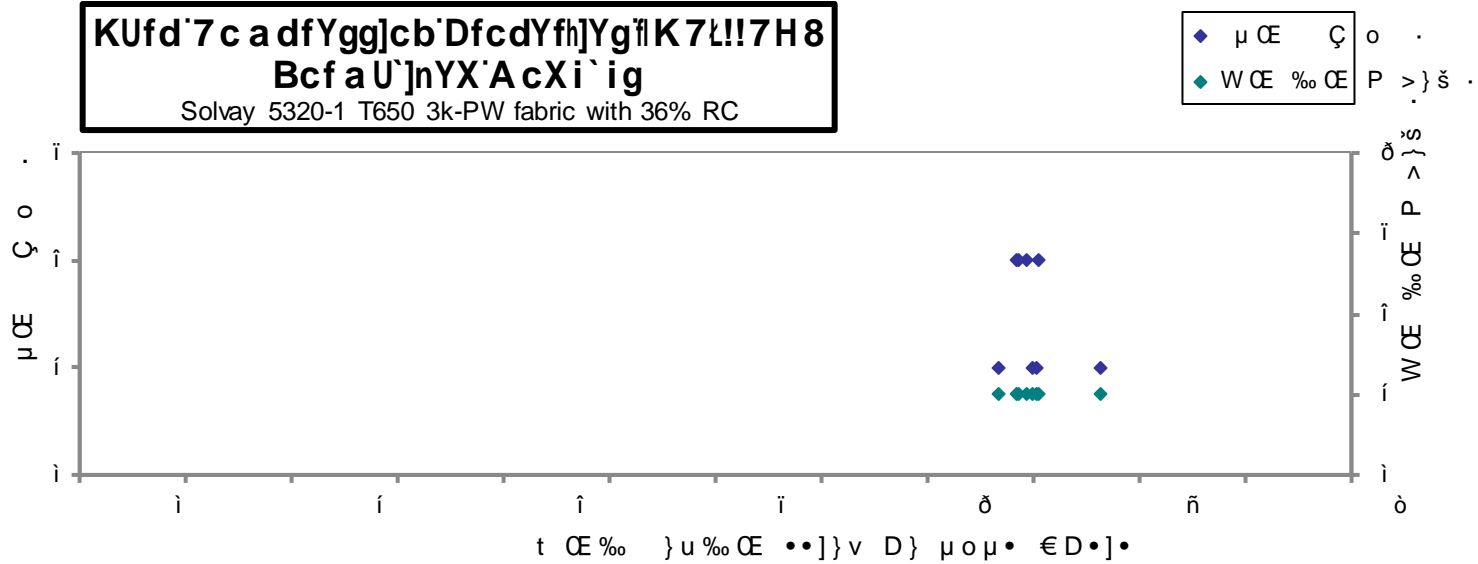
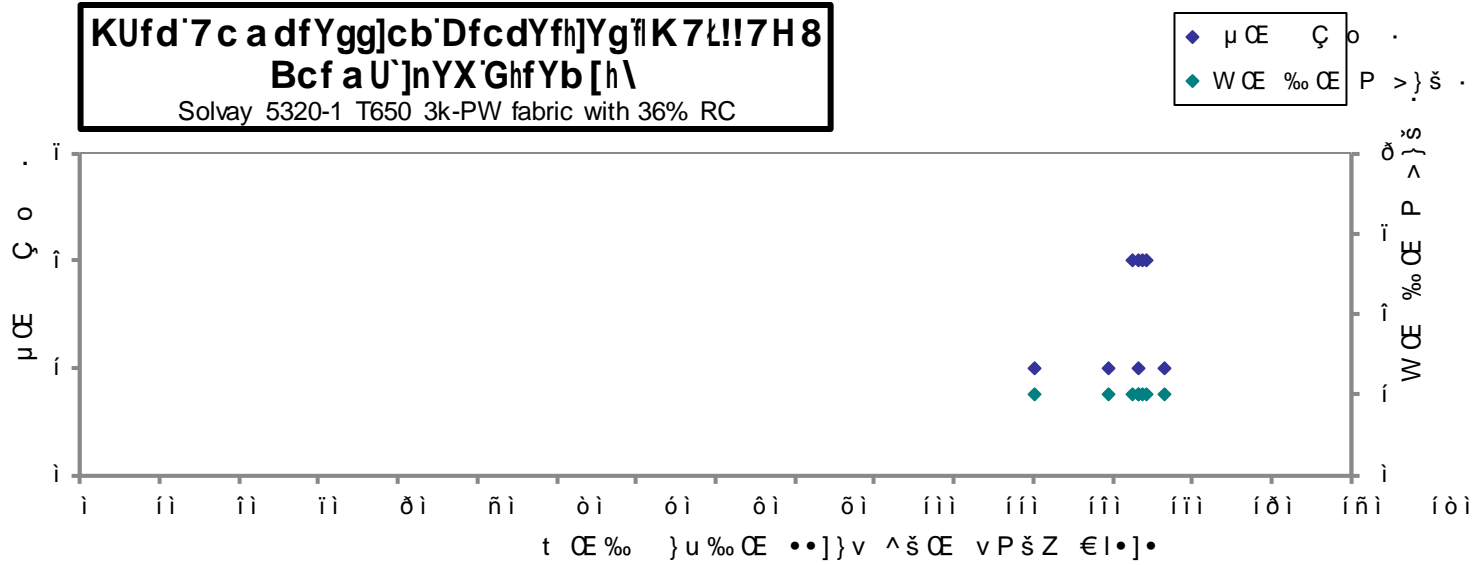
8YWY a VYf %-ž'&\$%-'

.....75 A!FD!&\$%-!\$( )'FYj'B#7

("' K Ufd'7c a dfYgg]cb'DfcdYfh]Yg'flK 7L'

b c f a U' n] b [  
h d m ' 0] b 0  
0.0077

GdYW]aYb'Bi a VYf	B-5F' 6UHW\'	B-5F' 7iFY'7mW'Y	DfYdfY['@ch' .	7iFY'7mW'Y' .	GhfYb[h\ 0_g]0	AcXi'ig' 0Ag]0	5j['' GdYW]aYb' H\]W_bYgg' 0]b0	'D]Yg]b' @Ua]bUrY	:U] ifY'AcXY	5j['''h d m ' 0] b 0	GhfYb[h\ b c f a ' 0_g]0	AcXi'ig' b c f a ' 0Ag]0
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-1	A	C1	1	1	122.677	9.211	0.113	15	BGM	0.0075	120.146	9.021
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-2	A	C1	1	1	138.578	9.126	0.114	15	BGM	0.0076	136.498	8.989
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-3	A	C1	1	1	135.480	8.806	0.114	15	BGM	0.0076	133.349	8.667



8YWy a VYf %-ž&\$%-

.....75 A!FD!&\$%-!\$( )'FYj'B#7

KUfd'7c a dfYgg]cb'DfcdYfh]Yg'fK 7L!FH8  
GhfYb[h\ /'AcXi'ig

b c f a U ] n ] b [ '  
h d m ' 0 ] b 0  
0.0077

GdYw]a Yb'Bi a VYf	B:5F' 6UhW\	B:5F' 7ifY'7mWY	DfYdfY['@ch' 7ifY'7mWY	GhfYb[h\ 0_g]0	AcXi'ig' 0Ag]0	5j[" GdYw]a Yb' H\]W_bYgg' 0]b0	'D]Yg]b' @Ua]bUhY	:U] ifY'AcXY	5j["'h d m ' 0 ] b 0	GhfYb[h\ b c f a ' 0_g]0	AcXi'ig b c f a ' 0Ag]0	
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-1*	A	C1	1	1	126.786	8.919	0.115	15	BGM	0.0076	125.890	8.856
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-2*	A	C1	1	1	122.642	8.946	0.115	15	BGM	0.0077	122.164	8.911
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-3	A	C1	1	1	126.631	9.322	0.114	15	BGM	0.0076	125.370	9.229
NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-4	A	C1	1	1	123.297	9.339	0.114	15	BGM	0.0076	121.980	9.239
NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-1*	A	C2	1	2	125.575	8.942	0.115	15	HAT, BAT	0.0076	124.723	8.881
NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-2***	A	C2	1	2		8.988	0.114	15	HIT	0.0076		8.898
NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-3	A	C2	1	2	114.577	9.007	0.115	15	BGM, HAT	0.0076	113.701	8.938
NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-4	A	C2	1	2	121.965	8.969	0.115	15	BGM, HAT	0.0076	120.926	8.893
NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-5***	A	C2	1	2	123.497		0.115	15	HAT, BGM	0.0076	122.553	

\*Modulus are averaged values of 2 strain gages.  
\*\*Strength not reported due to unacceptable failure mode.  
\*\*\*Specimen was not gaged, only strength is tested.

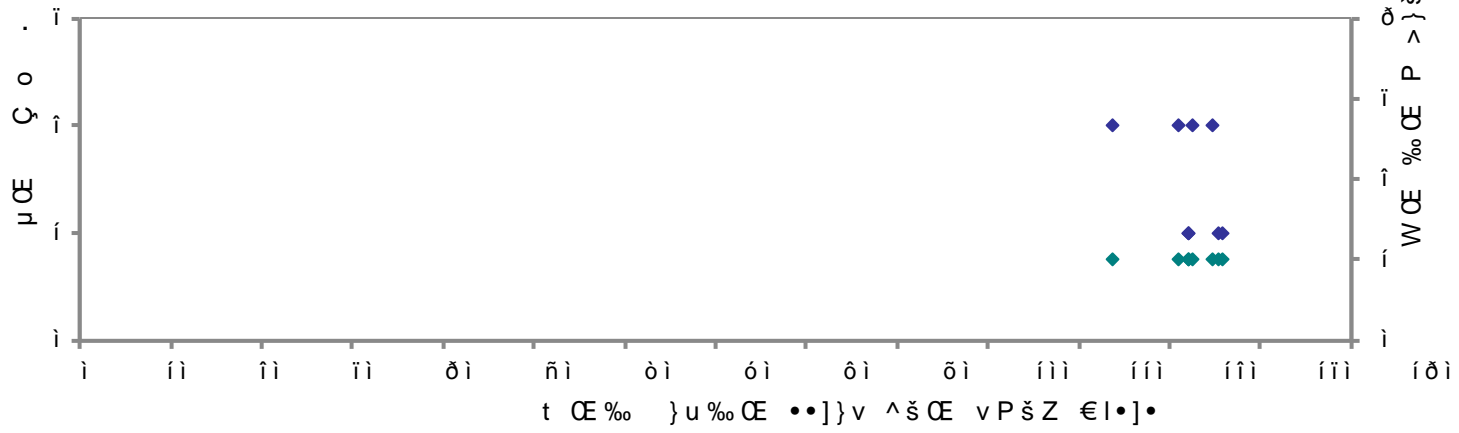
5jYFU[Y %&'%'&%	-'\$)(	5jYFU[Y b c f a '\$\$\$+'	%&&'%'	,'-,%
GhUbXUfX'8Yj'	'-\$%'	GhUbXUfX'8Yj' b c f a	'',)	\$%) ,
7cYZZ'cZ'JUf'0 i Q	'%*, %-\$-	7cYZZ'cZ'JUf'0 i Q b c f a	'%)*	%+%'
A]b'	%( ' ) ++	A]b'	'\$\$\$+'	%'**+\$%
AUI'	%&'**+, *	AUI'	'\$\$\$\$+	%'&' , -\$
Bi a VYf'cZ'GdYW'	,	Bi a VYf'cZ'GdYW'	-	,'

8YWy a VYf %-z'&\$%-'

.....75 A!FDI!&\$%-!\$( )'FYj'B#7

**KUfd'7c a dfYgg]cb'DfcdYfh]YgřilK7ł!!FH 8**  
**Bcf a U`]nYX'GhfYb [h\**  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

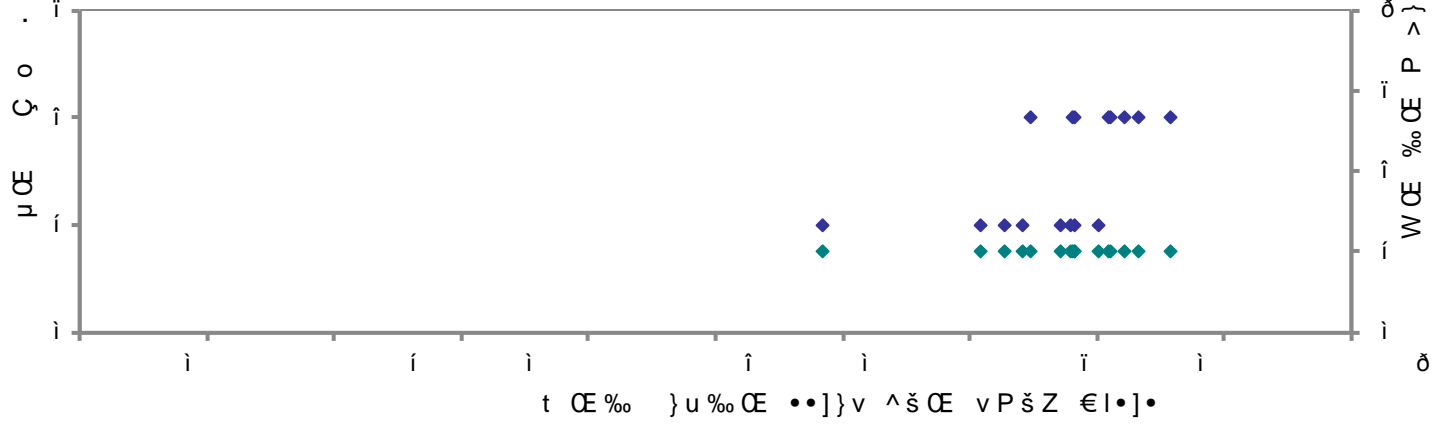
◆ μ CE Ç o .  
 ◆ W CE %o CE P > } .



8YWY a VYf'9

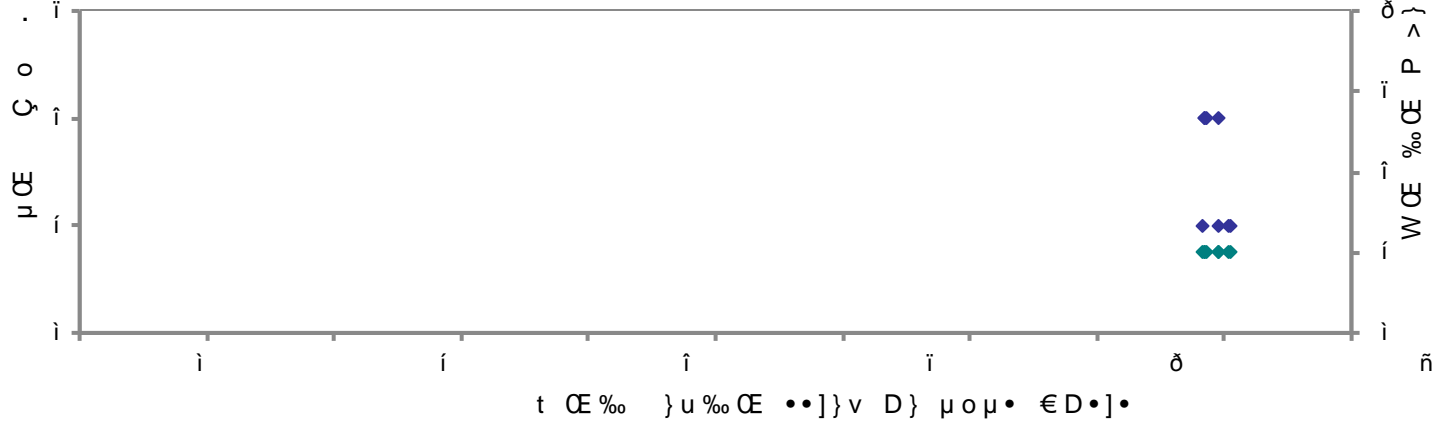
**KUfd'7c a dfYgg]cb'DfcdYfh]Ygfl K 7L!!9H K&  
 Bcf aU`nYX'GhfYb[h\  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC**

◆  $\mu_{CE}$   $\zeta$  o .  
 ◆  $W_{CE}$   $\%_{CE}$  P > } \$ .



**KUfd'7c a dfYgg]cb'DfcdYfh]Ygfl K 7L!!9H K&  
 Bcf aU`nYX'AcXi`ig  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC**

◆  $\mu_{CE}$   $\zeta$  o .  
 ◆  $W_{CE}$   $\%_{CE}$  P > } \$ .



8YWy a VYf %-ž&\$%- . . . . . \*\*\*\*\*75A!FD!&\$%-!\$( )'FYj'B#7

("(' :]``7c a dfYgg]cb`DfcdYfh]Yg`fl : 7L`

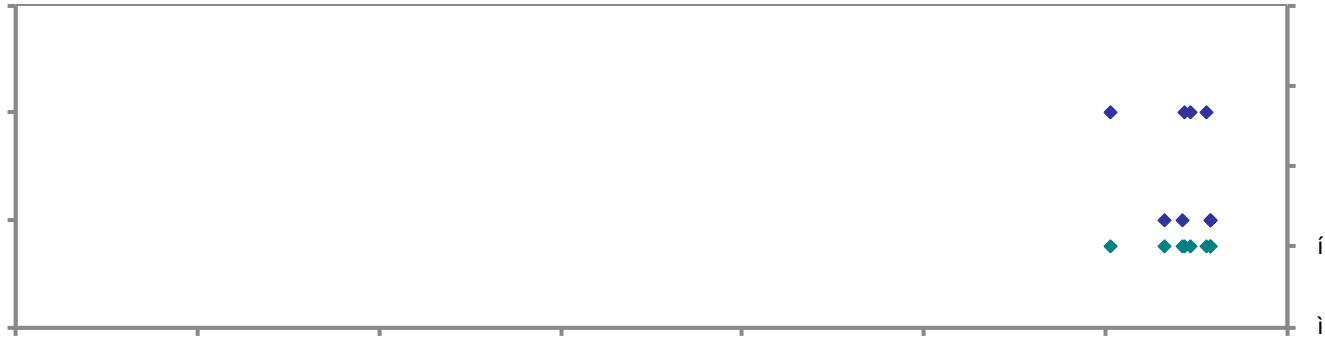
b c f a U`h]b[`  
h d m 0]b0  
0.0077

GdYw]a Yb`B i a VYf

B-5F` B-5F` DfYdfY[ '@ch`  
6UhW\` 7 i fY`7mW`Y`

8YWy a VYf %-ž&\$%-

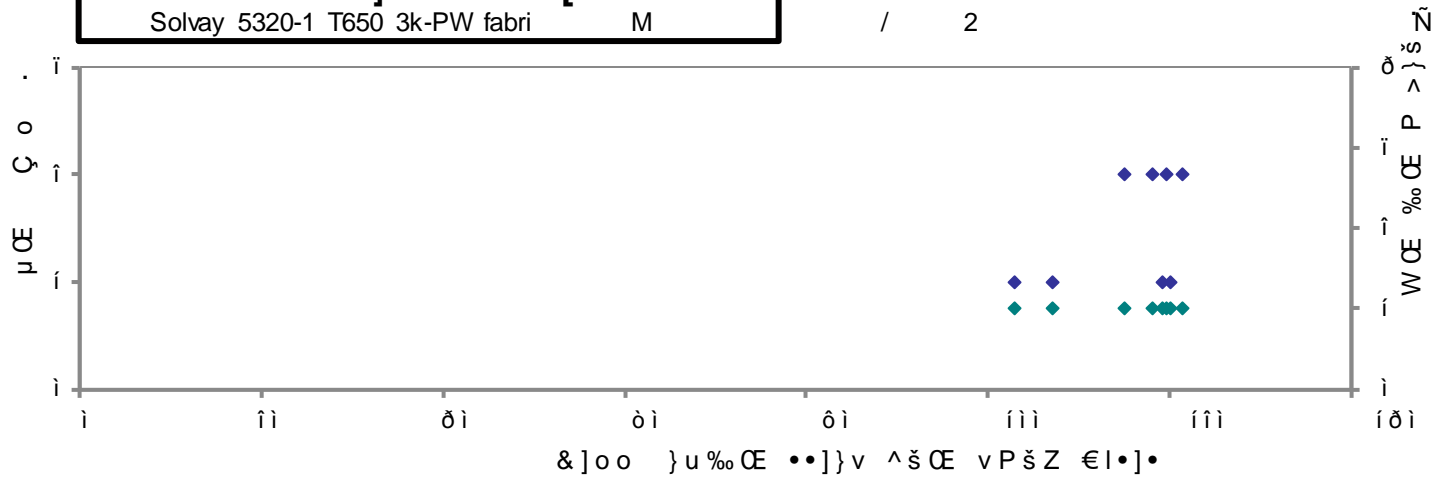
.....75 A!FD!&\$%-!\$( )'FYj`B#7







:]`7 c a dfYgg]cb`DfcdYfh]Ygñ: 7ł!!FH 8  
 Bcf a U`nYX`GhfYb [h\  
 Solvay 5320-1 T650 3k-PW fabri M / 2





8YWy a VYf %-ž&\$%-

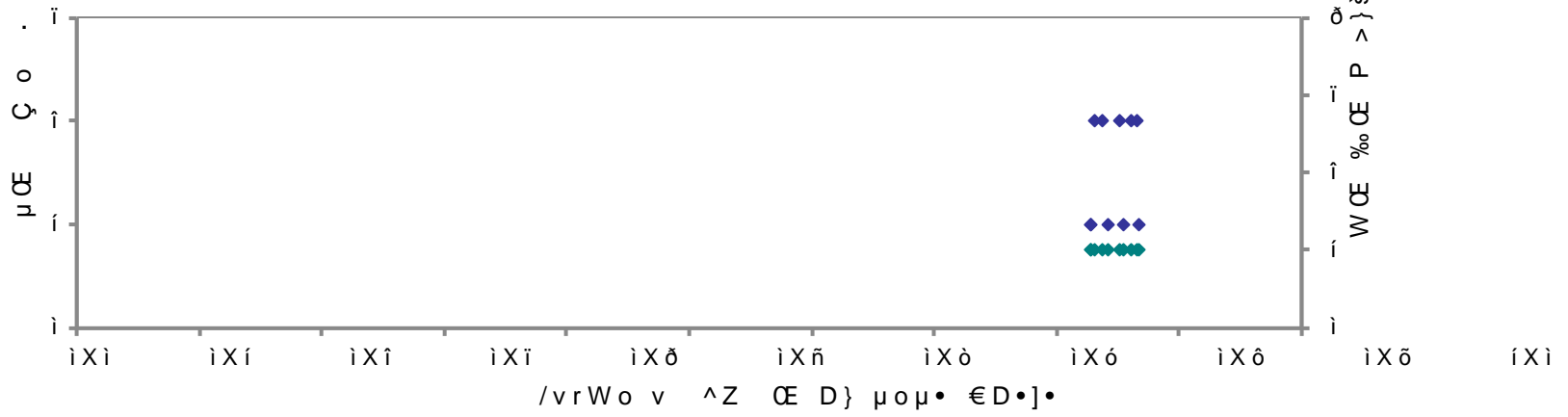
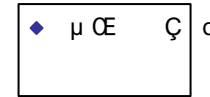
.....75 A!FD!&\$%-!\$( )'FYj`B#7







**=b!D`UbY'G\YUf'DfcdYfhjYgfl=DGL!!7H8**  
**AYUg ifYX'AcXi`ig**  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

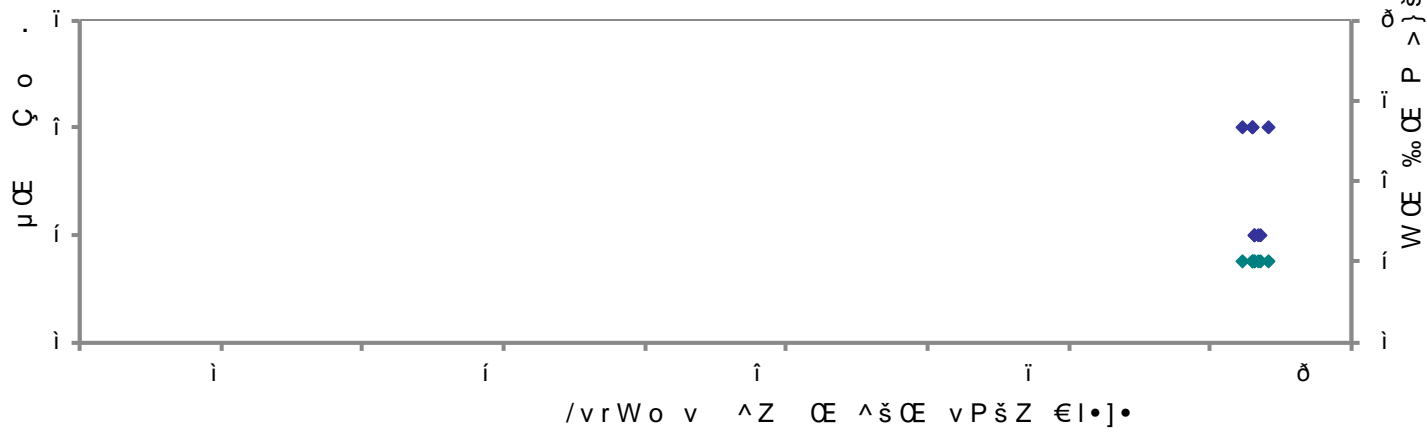






**=b!D`UbY`G\YUf`DfcdYfh]Ygřl=DGL!!FH 8**  
**A YUg i fYX`\$"& i `CZgYh`GhfYb[h\**  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

◆ μ OE Ç o .  
 ◆ W OE %o OE P > } š .



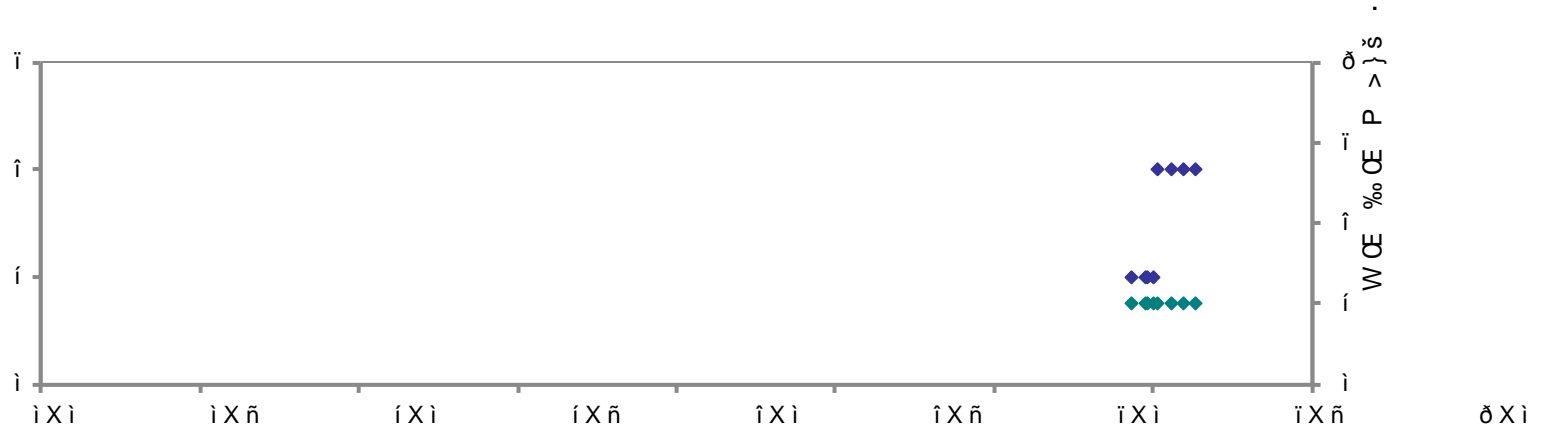
ñ



8YWy a VYf %-ž&\$%- ..... 75 A!FD!&\$%-!\$() `FYj`B#7



8YWy a VYf %-ž'&\$%-'





8YWY a VYf %-ž'&\$%- ' .....75 A!FD!&\$%-!\$( )' FY j' B#7

("\*' @U a ]bU'G\cfh!6YU a 'GhfYb [h\ 'DfcdYfh]Yg'fIG6GŁ'

**G\cfh!6YU a 'GhfYb [h\ 'DfcdYfh]Yg'fIG6GŁ!!7H8**  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

GdYW]a Yb'Bi a VYf	B-5F' 6UhW\ ' ı	B-5F' 7 i fY' 7mW'Y	DfYdfY[ '@ch' ı	7 i fY' 7mW'Y ı	GhfYb [h\ 0_g]0	5 j ["" GdYW] a Yb' H\]W_bYgg' 0]b0	'D]Yg']b' @U a ]bUhY	5 j [""hdfm'0]b0	:U] i fY' AcXY
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-1	A	C1	1	1	14.385	0.244	32	0.0076	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-2	A	C1	1	1	15.070	0.243	32	0.0076	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-3	A	C1	1	1	13.810	0.243	32	0.0076	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-4	A	C1	1	1	14.816	0.243	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-1	A	C2	1	2	13.845	0.246	32	0.0077	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-2	A	C2	1	2	14.250	0.245	32	0.0077	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-3	A	C2	1	2	14.227	0.245	32	0.0077	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-4	A	C2	1	2	14.444	0.246	32	0.0077	INTERLAMINAR SHEAR, TENSION

5 jYfU[Y %(')\* '\$\$\$+\*

GhUbXufX' 8Yj' \$(' ('

7cYZZ' cZ' JUF''0 i Q ''\$&&

A]b' %'',%\$ '\$\$\$+\*

AUI' %)'\$+\$ '\$\$\$++

Bi a VYf cZ' GdYW'' , ,



G \cfh!6YU a 'GhfYb[h\`DfcdYfh]Yg'f!G6GL!!FH8  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

GdYW]a Yb'Bi a VYf	B-5F' 6UhW\`	B-5F' 7 i fY'7mW'Y	DfYdfY['@ch	7 i fY'7mW'Y	GhfYb[h\ 0_g]Q	5 j[" GdYW]a Yb' H\]W_bYgg' 0]bQ	'D]Yg]b' @U a]bUhY	5 j["h_d'm'0]bQ	:U] i fY'AcXY
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-1	A	C1	1	1	12.760	0.243	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-2	A	C1	1	1	12.932	0.243	32	0.0076	INTERLAMINAR SHEAR, TENSION
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-3	A	C1	1	1	12.948	0.244	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-4	A	C1	1	1	12.945	0.243	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-1	A	C2	1	2	13.180	0.244	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-2	A	C2	1	2	12.887	0.244	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-3	A	C2	1	2	12.779	0.244	32	0.0076	INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-4	A	C2	1	2	13.433	0.244	32	0.0076	INTERLAMINAR SHEAR

5 jYfU[Y %&-', '  
 GhUbXUfX'8Yj' \$'&&' \$\$\$\$+\*  
 7cYZZ'cZ'JUf''0 i Q %'+% )  
 A]b' %&+\*\$ \$\$\$\$+\*  
 AUI' %''(' ' \$\$\$\$+\*  
 Bi a VYf cZ'GdYW" ,





GdYW]a Yb'Bi a VYf	B=5F' 6UhW\`	B=5F' 7 ifY'7mWY	DfYdfY[@ch' 7 ifY'7mWY'	GhfYb[h\ 0_g]Q	5 j[" GdYW]a Yb' H\]W_bYgg' 0]bQ	'D]Yg]b' @Ua]bUhY	5 j["h <sub>dm</sub> '0]bQ	:U] ifY'AcXY
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-1	A	C1	1	1	6.739	0.245	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-2	A	C1	1	1	6.762	0.244	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-3	A	C1	1	1	6.859	0.244	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-4	A	C1	1	1	6.866	0.244	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-1	A	C2	1	2	7.391	0.245	32	0.0077 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-2	A	C2	1	2	7.087	0.245	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-3	A	C2	1	2	6.929	0.244	32	0.0076 INTERLAMINAR SHEAR
NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-4	A	C2	1	2	6.923	0.244	32	0.0076 INTERLAMINAR SHEAR

5 jYfU[Y \*\*-( )  
 GhUbXufX'8Yj\* \$&%\$  
 7cYZZ" cZ'JUf"0 i Q '\$&\$\*  
 A]b\* \*\*+ ' -  
 AUl' +'' -%  
 Bi a VYf cZ'GdYW" ,  
 \$\$\$+\*  
 \$\$\$+\*  
 \$\$\$++  
 , H + -' 0

8YWy a Vyf %-z &\$ %-

.....75 A!FD!&\$-!\$( )`FYj`B#7





8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )`FYj`B#7

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )'FYj`B#7

bcfaU]n]b[  
h<sub>d</sub>m'0]b0  
0.0077

GdYW]aYb`Bi aVYf

B-5F'  
6UHW\`

B-5F'  
7ifY'7mWY

DfYdfY['@ch-B h'

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )'FYj`B#7



8YWy a VYf %-ž'&\$%-'





8YWy a VYf %-ž'&\$%-'

.....75A!FD!&\$%-!\$( )'FYj`B#7

bcaU']nb[  
h\_d'm'0]b0  
0.0077

GdYW]a Yb`Bi a VYf

B-5F'  
6UhW\`

B-5F'  
7ifY'7mWY

DfYdfY['@ch' 7ifY'7mWY'

GhfYb[h\  
0\_g]R

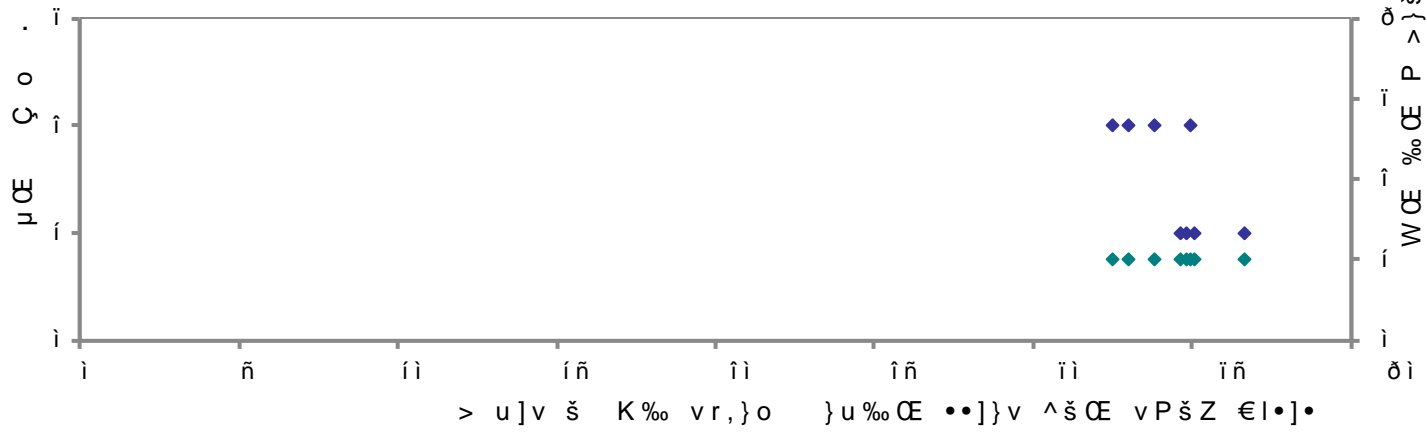
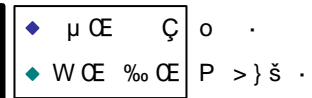
5j["  
GdYW]a Yb`  
H\]W\_bYgg'  
0]b0

`D]Yg]b`  
@Ua]bUhY

:U]ifY`AcXY

5j["h\_d'm'0]b0

**@U a ]bUhY`CdYb!<c`Y`7c a dfYgg]cb`DfcdYfh]Yg`flC<7%k!!9HK&**  
**Bcf aU`nYX`GhfYb [h\**  
 Solvay 5320-1 T650 3k-PW fabric with 36% RC



8YWy a VYf %-ž'&\$%-'

.....75 A!FD!&\$%-!\$( )'FYj'B#7

("-' Í&#)\$&#) Î'7c a dfYgg]cb'GhfYb [h\ '5ZhYf'= a dUWh'% 'DfcdYfh]Yg'fl75=%k'

<p>@Ua]bUhY'7c a dfYgg]cb'5ZhYf'= a dUWh'% 'DfcdYfh]Yg'fl75=%k!!FH8</p> <p>GhfYb[h\</p> <p>Solvay 5320-1 T650 3k-PW fabric with 36% RC</p>
--

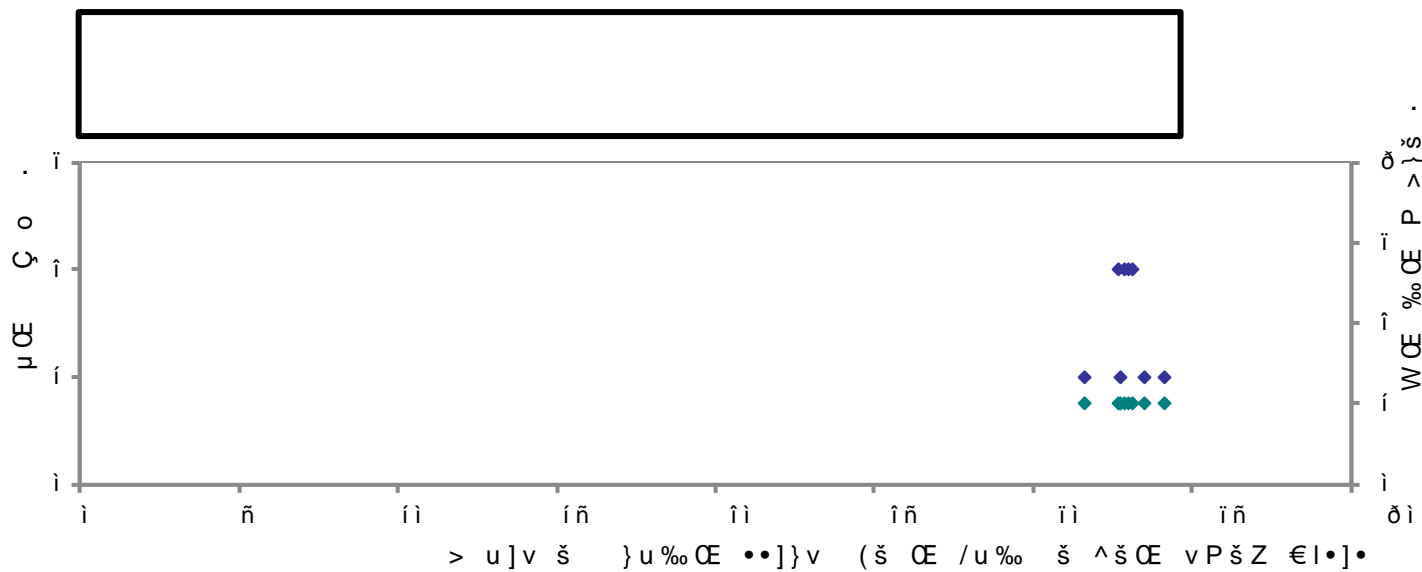
bcf a U]n]b [
h_d m'0]b0
0.0077

GdYW]a Yb'Bi a VYf	B=5F' 6UhW\`	B=5F' 7ifY'7mW'Y	DfYdfY['@ch	7ifY'7mW'Y	GhfYb[h\ 0_g]0	AYUg ifYX' = a dUWh' 9bYf [m 0]b'VZ0	5j ['' GdYW]a Yb' H\W_bYgg' 0]b0	'D]Yg]b' @Ua]bUhY	:U] ifY'AcXY
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-1	A	C1	1	1	34.241	273.46	0.184	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-2	A	C1	1	1	32.716	280.41	0.185	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-3	A	C1	1	1	31.537	277.66	0.185	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-4	A	C1	1	1	33.465	280.03	0.185	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-1	A	C2	1	2	32.504	280.79	0.186	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-2	A	C2	1	2	32.908	280.37	0.186	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-3	A	C2	1	2	32.905	280.17	0.185	24	LDM
NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-4	A	C2	1	2	32.713	280.07	0.186	24	LDM

5j [''h_d m'0]b0	GhfYb[h\bcfa' 0_g]0
0.0077	34.104
0.0077	32.716
0.0077	31.583
0.0077	33.478
0.0077	32.700
0.0077	33.115
0.0077	33.008
0.0077	32.841

5jYfU[Y '&',+'  
 GhUbXUfX'8Yj" '\$'++(  
 7cYZZ'cZ'JUf''0 i 0 &'') )  
 A]b" '%)'+'  
 AU1" '(&(%  
 Bi a VYf'cZ'GdYW" ,

5jYfU[Ybcfa \$\$\$++ '&'-'  
 GhUbXUfX'8Yj'bcfa '\$'+&  
 7cYZZ'cZ'JUf''0 i 0bcfa &'%, ,  
 A]b" '\$\$\$++ '%)', '  
 AU1" '\$\$\$++ '(%\$(\$  
 Bi a VYf'cZ'GdYW" , ,



)" 5XX]h]cbU`7 c a dfYgg]cb`5ZhYf`= a dUWh`8UhU`

Impactor Diameter: 0.625"

Representative of Damage Area:



Damage Area and Dent Depth Summary:

GdYW] a Yb`8`	8U a U[Y`5fYU f]bW\&L`	8Ybh`8Ydh\` f]bW\&L`
NTP-5325QR1-SOL-S36-NIAR-CAI1-A-C1-1-RTD-1	0.0335	1.179
NTP-5325QR1-SOL-S36-NIAR-CAI1-A-C1-1-RTD-2	0.0375	1.403



8YWy a VYf %-ž&\$%- . . . . . 75A!FD!&\$%-!\$( )'FYj`B#7

\*''` KUfd`7c a dfYgg]cb`Ë`FH8`




8YWy a VYf %-ž&\$%- .....75 A!FD!&\$%-\$() FYj B#7

\*") =b!D`UbY`G\YUf`E`FH8`

8YWy a VYf %-ž&\$%- .....75A!FD!&\$%-!\$( )'FYj'B#7

+'' Ac]gh i fY'7cbX]h]cb]b[ '7\Ufhg'

+ "%' =b!D`UbY`G\YUf`Ë`H\]bbYgh`DUbY`

, " 8A5'FYgi'hg'

<b>8A5'FYgi'hg'Gi a aUfm'! : 55'FYdU]f' E i U'Z]WUh]cb BHD!) '&amp;)EF=!GC@!G' *!B=5F' 8A5'8fm'fl9e i ]jU'YbWmł</b>				
GUad'Y'	CbgYh'GhcfU[Y'AcXi'ig		DYU_cZHUb[Ybhi'8Y'hU	
	H <sub>i</sub> '0š7Q	H <sub>i</sub> '0š:Q	H <sub>i</sub> '0š7Q	H <sub>i</sub> '0š:Q
CAI1-A-C1-1-DMA-D	200.52	392.94	214.27	417.69
CAI1-A-C2-1-DMA-D	201.11	394.00	214.75	418.55
FC-A-C1-1R-DMA-D	202.72	396.90	220.27	428.49
FC-A-C2-1R-DMA-D	203.52	398.34	221.87	431.37
FT-A-C1-1R-DMA-D	203.11	397.60	220.73	429.31
FT-A-C2-1R-DMA-D	203.50	398.30	220.38	428.68
IPS-A-C1-1-DMA-D	195.17	383.31	211.41	412.54
IPS-A-C2-1-DMA-D	195.76	384.37	212.33	414.19
OHC1-A-C1-1-DMA-D	201.98	395.56	218.12	424.62
OHC1-A-C2-1-DMA-D	199.54	391.17	214.49	418.08
OHT1-A-C1-1-DMA-D	198.05	388.49	215.18	419.32
OHT1-A-C2-1-DMA-D	198.29	388.92	215.73	420.31
SBS-A-C1-1-DMA-D	204.73	400.51	215.03	419.05
SBS-A-C2-1-DMA-D	203.12	397.62	215.32	419.58
WC-A-C1-1-DMA-D	198.89	390.00	214.72	418.50
WC-A-C2-1-DMA-D	201.47	394.65	218.48	425.26
WT-A-C1-1-DMA-D	198.79	389.82	214.59	418.26
WT-A-C2-1-DMA-D	199.99	391.98	216.46	421.63
Average	200.57	393.03	216.34	421.41
Standard Deviation	2.73	4.91	2.97	5.35

<b>8A5'FYgi'hg'Gi a aUfm'! : 55'FYdU]f' E i U'Z]WUh]cb BHD!) '&amp;)EF=!GC@!G' *!B=5F' 8A5'KYh'fl9e i ]jU'YbWmł</b>				
GUad'Y'	CbgYh'GhcfU[Y'AcXi'ig		DYU_cZHUb[Ybhi'8Y'hU	
	H <sub>i</sub> '0š7Q	H <sub>i</sub> '0š:Q	H <sub>i</sub> '0š7Q	H <sub>i</sub> '0š:Q
CAI1-A-C1-1-DMA-W	159.01	318.22	173.93	345.07
CAI1-A-C2-1-DMA-W	158.37	317.07	173.89	345.00
FC-A-C1-1R-DMA-W	156.99	314.58	171.16	340.09
FC-A-C2-1R-DMA-W	156.41	313.54	170.95	339.71
FT-A-C1-1R-DMA-W	157.59	315.66	171.43	340.57
FT-A-C2-1R-DMA-W	158.82	317.88	171.78	341.20
IPS-A-C1-1-DMA-W	145.98	294.76	167.39	333.30
IPS-A-C2-1-DMA-W	145.64	294.15	167.56	333.61
OHC1-A-C1-1-DMA-W	157.96	316.33	173.93	345.07
OHC1-A-C2-1-DMA-W	156.79	314.22	172.69	342.84
OHT1-A-C1-1-DMA-W	156.63	313.93	171.93	341.47
OHT1-A-C2-1-DMA-W	157.01	314.62	173.29	343.92
SBS-A-C1-1-DMA-W	161.88	323.38	174.23	345.61
SBS-A-C2-1-DMA-W	161.14	322.05	174.30	345.74
WC-A-C1-1-DMA-W	158.02	316.44	171.82	341.28
WC-A-C2-1-DMA-W	158.83	317.89	172.98	343.36
WT-A-C1-1-DMA-W	157.61	315.70	170.59	339.06
WT-A-C2-1-DMA-W	157.38	315.28	171.15	340.07
Average	156.78	314.21	171.94	341.50
Standard Deviation	4.25	7.64	2.03	3.66

8YWy a VYf %-ž&\$%-`

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$( )`FYj`B#7